

## Binary mixtures of two anionic polysaccharides simulating the rheological properties of oxidised starch\*\*

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**Abstract.** Modifications of starches are carried out to improve their industrial usefulness. However, the consumers prefer natural products. For this reason, various methods of starch properties modification are applied to replace those requiring the use of chemical reagents. The aim of this study was to determine whether it is possible to use binary pastes, containing normal potato starch and xanthan gum, as substitutes of chemically modified starches (with oxidised starch E 1404 pastes as an example). Flow curves with hysteresis loops, apparent viscosity at constant shear rate of 50 s<sup>-1</sup> and in-shear structural recovery test with pre-shearing were applied to study the rheological properties of the pastes. It was found that two anionic hydrocolloids, potato starch and xanthan gum, can form binary systems with thickening properties, provided that their proportions are adequately adjusted. Some of the binary pastes under investigation exhibited rheological properties resembling pastes of starch oxidised with hypochlorite (E 1404). The way of tailoring the binary pastes properties is presented.

**Keywords:** oxidised starch, potato starch, rheological properties, xanthan gum

### INTRODUCTION

Developments in food technology, changes in culinary habits among populations and attempts at limiting the energetic value of meals, evoked a demand for novel texturing agents for food. Such agents should also conform to regulations associated with digestibility, health precautions, storage stability and resistance to microorganisms. There are several possibilities to meet, at least in part, demands of this kind. Thus, selection among polysaccharide hydrocolloids seems to be the most obvious.

In the case of starches, both their physicochemical and functional properties depend on the selection of starch of a given botanical origin (Singh *et al.*, 2003; Swinkels, 1985; Tegge, 2010; Whistler and BeMiller, 1977). Rheological and textural properties of pastes and gels of a given starch are determined by the pasting regime, *eg* concentration, time and temperature, all influencing the degree of pasting and accompanying degradation of amylose and amylopectin chains (Appelqvist and Debet, 1997; Sikora *et al.*, 2015; Tomasik and Schilling, 1998a, 1998b). Also, the rheological properties of starch systems are dependent on the pH and temperature changes as well as on mechanical forces (Arocas *et al.*, 2009; Kaur *et al.*, 2012; Rutkowski *et al.*, 2003).

In order to enhance the industrial suitability of starches, their modifications are undertaken. They can be chemical, physical, enzymatic (or combinations of them), resulting in a notable number of starch derivatives (Kaur *et al.*, 2012; Pietrzyk and Fortuna, 2006; Tegge, 2010). However, national food laws of most countries put some limits on the levels of chemically modified starches (for instance, oxidised, starch, starch phosphates, esters of starch with organic acids, etherified starch and so on) for nutritional purposes (Compendium, 2011; Le Than *et al.*, 2007).

Oxidised starch (OS), with code number E 1404, is produced by the action of sodium hypochlorite over normal starch. OS is commonly used as a thickener, stabiliser and emulsifier in various types of food (Compendium, 2011; Rutkowski *et al.*, 2003). It should not be used without any limit. According to the Codex Alimentarius (2014), the daily intake limit for infants and youngsters should not exceed

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5 000 mg kg<sup>-1</sup> body weight. It is one of the reasons of some distrust towards that food ingredient and this point of view spreads onto other chemically modified food additives. That argument rationalises the attempts at looking for their substitutes.

Recently, binary hydrocolloid systems evoked considerable interest as filling, thickening and texturising agents (Alloncle *et al.*, 1989; Arocas *et al.*, 2009; Kowalski *et al.*, 2008; Sikora *et al.*, 2010 and references therein). Such binary hydrocolloid blends could be tailored, provided that interactions between polysaccharides in such mixtures are properly recognised (Kowalski *et al.*, 2008). Morris (1991) distinguished four types of networks formed in binary hydrocolloid mixtures depending on interactions between the components.

They were:

- network formed of one hydrocolloid and a second hydrocolloid (non-gelled) entrapped inside that network;
- network formed by both hydrocolloids which built independent mutually interpenetrating networks;
- network of both hydrocolloids paste separating into two phases, and
- a coupled, common network.

The botanical origin of starch as a component of such mixtures is crucial, as the hydrocolloids used can be electrically either neutral or ionic (Ramsden, 2004). Normal potato starch (NPS) is the sole anionic starch. Therefore, on blending NPS with other anionic polysaccharides a decrease in viscosity of resulting blends can be observed. Such behaviour was documented in the case of blends of NPS and xanthan gum (XG) (Kowalski *et al.*, 2008). Nevertheless, binary NPS-XG systems have been fairly intensively studied (Baranowska *et al.*, 2008; Krystyjan *et al.*, 2013; Mandala *et al.*, 2002; Sikora *et al.*, 2008b) and used with success in thickening desserts, sauces and syrups (Sikora *et al.*, 2007, 2008a). However, there is no research found in the literature that aims at comparison of the thickening properties of NPS-XG blends with those of OS pastes.

The aim of the study presented in this paper was to investigate binary NPS pastes containing small amounts of xanthan gum. A way of tailoring the properties of NPS-XG binary pastes for using them as substitutes of chemically modified starches is discussed, taking oxidised starch E 1404 (OS) pastes as an example, thus pointing to the possibility of OS (E 1404) substitution with NPS-XG binary mixtures.

#### MATERIALS AND METHODS

Normal potato starch (NPS) was isolated from potatoes of the Tajfun variety, purchased from the Experimental Station of Variety Evaluation in Węgrzce, Poland. The starch contained 86.92% dry mass, 111.9 mg 100 g<sup>-1</sup> d.m. total phosphorus, 0.13% fat and 31.99% amylose. Its aqueous

solubility was 14.66 and 20.94% at 80 and 95°C, respectively. Water binding capacity of that starch was estimated at 37.34 and 69.34 g l<sup>-1</sup> g d.m. at 80 and 95°C, respectively. Oxidised starch (OS) (LU-1404-1) was purchased from WPPZ S.A. in Luboń, Poland. It was prepared by oxidation of potato starch with sodium hypochlorite. Xanthan gum (XG) from *Xanthomonas campestris* (G1253-500G, Lot#100M0218V) was purchased from Sigma-Aldrich (St. Louis, USA).

Suspensions of 2, 3, 4 and 5% (d.m.) NPS containing XG at concentrations of 0, 0.010, 0.075 and 0.150% were placed in 100 cm<sup>3</sup> beakers and supplemented with distilled water to a total weight of 100 ± 0.00 g. The suspensions were agitated for 10 min at room temperature, at 400 r.p.m., followed by 30 min of heating and stirring at 400 r.p.m. in a water bath at either 80 or 95°C. Suspensions of 2-5% (d.m.) OS were agitated at 400 r.p.m. at room temperature for 10 min and then heated with continuous stirring (400 r.p.m.) at 95°C for 30 min. Pasting of OS samples only at 95°C aimed at simulating conditions similar to the industrial ones (cooking), while the pastes of NPS were heated both at 80 and 95°C, which was aimed at the acquisition of various pastes with an addition of XG, differentiated by rheological properties, and in this way at the enhancement of the probability of producing pastes with rheological properties resembling those of OS properties.

A rheometer, RheoStress RS 1 (Gebreuder Haake GmbH, Karlsruhe, Germany), was used. It operated with a measuring system consisting of two coaxial cylinders Z41 Ti. Temperature of 50°C was maintained during the measurements. The measurements were run in duplicates.

In the hysteresis loop test with the rheometer RS 1 at controlled shear rate, within 600 s an increase from 0.1 to 300 s<sup>-1</sup> followed by 120 s maintaining constant shear rate at 300 s<sup>-1</sup> and a decrease in the shear rate from 300 to 0.1 s<sup>-1</sup> within 600 s were noted. The areas of the hysteresis loop were calculated by summation of the areas of trapeziums situated between ascending and descending curves. The power of thixotropy in the volume of the sample was calculated as a function of the shear rate (Sikora *et al.*, 2015). Rheological properties were analysed by fitting the Ostwald – de Waele rheological model (1) to the flow curves taken at shear rate increasing from 0 to 300 s<sup>-1</sup>:

$$\tau = k \dot{\gamma}^n,$$

where:  $\tau$  is the shear stress (Pa),  $K$  is the consistency coefficient (Pa s<sup>n</sup>),  $\dot{\gamma}$  is the shear rate (Pa s<sup>-1</sup>), and  $n$  is the flow behaviour index. The estimations were duplicated.

In-shear structural recovery test with pre-shearing was carried out according to the procedures of Mezger (2002), Achayuthakan and Supphantharika (2008), Wang *et al.* (2009; 2010), modified by Sikora *et al.* (2015), as follows: 1) pre-shearing – a constant shear rate of 100 s<sup>-1</sup> for 30 s, 2) relaxation – a zero shear rate for 300 s, 3) a constant shear rate

of  $1 \text{ s}^{-1}$  for 120 s, 4) a constant shear rate of  $300 \text{ s}^{-1}$  for 60 s, 5) a constant shear rate of  $1 \text{ s}^{-1}$  for 240 s. The results enabled calculations of the degree of structure recovery (DSR) of the pastes according to Wang *et al.* (2009; 2010) – the ratio of the average apparent viscosity in the fifth (obtained in the first 120 s) and the third step were considered.

Apparent viscosity was taken within 10 min at constant shear rate of  $50 \text{ s}^{-1}$ .

Statistica 12.0 (Statsoft, Tulsa, OK., USA) involving one- and two-way analysis of variance (ANOVA) was applied. Significant differences at  $\alpha = 0.05$  were indicated using Duncan's test.

## RESULTS AND DISCUSSION

As shown in Table 1, consistency coefficients  $K$  and flow behaviour indices  $n$  of the NPS pastes prepared at given temperature, that is either 80 or 95°C, increased with the concentration of NPS in the paste.

Consistency coefficient ( $K$ ) and flow behaviour index ( $n$ ) depended on the NPS paste concentration as well as on the temperature of the paste preparation. Thus, in 2 and 3% NPS pastes, as temperature of pasting increased from 80 to 95°C the consistency of the paste increased. It could reflect a higher degree of swelling and pasting of starch granules. However, in more concentrated 4 and 5% NPS pastes  $K$  decreased with an increase in pasting temperature. It could reflect the effect of water deficiency obstructing complete pasting of granules. That effect was confirmed in our recent paper (Sikora *et al.*, 2015). Flow behaviour indices,  $n$ , increased with an increase in temperature of pasting and the pastes concentration.

The effect of admixture of XG to NPS pastes depended on the amount of XG added, NPS paste concentration and temperature of the paste preparation. Admixture of XG to the pastes prepared at 80 and 95°C always resulted in an increase in the consistency coefficient  $K$  and simultaneous decrease in the flow behaviour index  $n$ . As documented by Table 1, the sensitivity of these parameters to admixture of XG depended on the NPS paste concentration. However, these effects on  $K$  and  $n$  parameters were linear neither against the NPS paste concentration, concentration of admixed XG nor temperature of the NPS paste preparation.

Pastes without XG exhibited some thixotropy. Generally, it ceased with an increase in the paste concentration and pasting temperature. Admixture of XG almost always eliminated thixotropy (Table 1), however a clear opposite effect was observed in the case of 5% pastes prepared at 80°C.

Such results (non linear changes of  $K$  and  $n$  values and thixotropic properties) could be rationalised in terms of cooperation of at least two phenomena whose dominant role depended on concentration of NPS in the pastes and addition of XG. One of them could be an effect of water deficiency. Undoubtedly, pasting of 2% binary pastes

could be completed to a highest extent and hence enveloping swollen starch granules with XG (Hermansson *et al.*, 1995) could be the least essential. Its role likely increased with the paste concentration and was supported by lower pasting temperature. Hence, the influence of enveloping non-pasted granules with XG could be met in 5% binary paste prepared at 80°C. This effect could be responsible for considerable increase in thixotropy of those pastes (Table 1). Unexpectedly, only some 5% binary pastes exhibited residual thixotropy. Likely, other effects associated with the formation of binary paste structures (Morris, 1991) could be involved. Thorough inspection of the irregularities in thixotropy/antithixotropy of binary pastes in terms of the concentration of admixed XG might support this point of view. The most frequent irregularities in the thixotropy/antithixotropy magnitudes were encountered for the pastes containing 0.010 and 0.075% XG. One could assume that the smallest amount (0.010%) of XG in binary pastes produced uniform paste macrostructure of reduced consistency and increased flow due to either disorder caused by entrapped XG or the formation of a coupled common paste (Morris, 1991). An increase in the concentration of XG up to around 0.075% could provide a network formed of two separated phases. At XG concentration exceeding 0.075%, a system of independent mutually interpenetrating networks could be formed.

Apparent viscosity of binary NPS-XG pastes was also one of their characteristic properties. These taken at constant shear rate ( $50 \text{ s}^{-1}$ ) appeared fairly stable in time. Their average values depended on the concentration of NPS and XG as well as on the temperature of the paste preparation (Table 2).

Generally, the average apparent viscosity values of 2-4% NPS prepared at 80°C decreased upon an addition of XG independently on its concentration, while this parameter of the 5% NPS increased with the addition of 0.010 and 0.075% XG and decreased upon the addition of 0.150% XG. Such an irregularity can be explained in terms of competition for water molecules in water-deficient systems.

The apparent viscosity of 3-5% NPS prepared at 95°C decreased upon an addition of XG independently on its concentration, while in the 2% NPS an increase upon the addition of 0.075 and 0.150% XG and decrease upon the addition of 0.010% XG was observed. Noted irregularities resulted from low concentration of the whole system in which the apparent viscosity was dependent on the casual location of the XG molecules in the bulk system (Mandala *et al.*, 2002; Sikora *et al.*, 2015). It seems that pasting of 2% NPS-XG pastes was highly completed and hence enveloping swollen starch granules with XG was not so important (Hermansson *et al.*, 1995).

**Table 1.** Parameters of the rheological Ostwald – de Waele model and area of the hysteresis loop for pastes of potato starch (NPS) without and with the xanthan gum (XG) admixture

Pasting temperature (°C)	XG concentration (%)	Ostwald – de Waele model*		Hysteresis loop area ( $W\ m^{-3} = Pa\ s^{-1}$ )		
		$K$ ( $Pa\ s^n$ )	$n$	Thixotropy	Antithixotropy	Total area
2% pastes						
80	0	1.42±0.17de**	0.525±0.015b	90±17a	0±0c	90±17b
	0.010	1.36±0.18e	0.515±0.011b	27±6bcd	3±1c	30±4b
	0.075	2.08±0.07bc	0.342±0.003cd	53±1b	0±0c	53±1b
	0.150	2.34±0.02a	0.274±0.001d	40±6bc	0±0c	40±6b
95	0	0.82±0.05f	0.723±0.013a	22±8cd	224±40a	246±33a
	0.010	1.72±0.36cde	0.576±0.077b	20±28cd	78±59b	98±88b
	0.075	1.80±0.08cd	0.405±0.012c	2±1d	43±11bc	45±10b
	0.150	2.33±0.21b	0.332±0.019d	0±0d	75±17b	75±17b
3% pastes						
80	0	3.22±0.10bc	0.529±0.016b	93±71a	53±8c	146±79bc
	0.010	4.44±0.60ab	0.464±0.011c	0±0b	165±28abc	165±28abc
	0.075	4.77±0.21ab	0.363±0.007d	0±0b	157±40bc	157±40abc
	0.150	4.95±0.25ab	0.302±0.004e	0±0b	84±4c	84±4c
95	0	4.71±0.26ab	0.530±0.015b	33±8b	158±101bc	191±93abc
	0.010	2.15±0.73c	0.643±0.047a	1±1b	443±99ab	444±98ab
	0.075	6.59±1.12a	0.407±0.005d	3±1b	483±303a	486±302a
	0.150	5.67±2.07a	0.354±0.041de	0±0b	323±140abc	323±140abc
4% pastes						
80	0	7.13±0.74ab	0.550±0.016b	0±0b	508±24c	508±24c
	0.010	5.52±1.57bc	0.562±0.044b	0±0b	884±59ab	884±59ab
	0.075	6.85±0.82ab	0.443±0.019c	0±0b	800±109b	800±109b
	0.150	9.16±0.07a	0.322±0.001d	2±0a	153±11d	155±11d
95	0	2.72±0.37d	0.705±0.021a	2±1a	1086±79a	1088±78a
	0.010	3.37±1.31cd	0.659±0.058a	1±1ab	931±263ab	932±262ab
	0.075	6.77±1.71ab	0.472±0.042c	0±0b	241±105cd	241±105cd
	0.150	6.54±0.32b	0.420±0.011c	0±0b	270±13cd	270±13cd
5% pastes						
80	0	7.79±0.36de	0.587±0.006b	1±0a	983±76b	984±76b
	0.010	10.24±0.96bc	0.530±0.009c	421±322a	256±202c	677±120b
	0.075	11.40±0.01ab	0.448±0.004d	163±136a	399±93c	562±43b
	0.150	13.05±0.05a	0.369±0.011e	778±950a	179±244c	956±706b
95	0	4.92±0.27f	0.675±0.009a	4±5a	1720±128a	1723±123a
	0.010	4.54±0.06f	0.678±0.007a	0±0a	2128±337a	2128±337a
	0.075	6.10±0.06ef	0.576±0.011b	1±1a	1940±311a	1941±310a
	0.150	8.75±1.81cd	0.476±0.030d	0±0a	2184±42a	2184±42a

\* $K$  – consistency coefficient,  $n$  – flow behaviour index. In all cases correlation coefficient was in the range of  $R^2 > 0.996$ . \*\*Different characters in columns (for each starch concentration) point to statistically essential differences at  $\alpha = 0.05$ .

**Table 2.** Average apparent viscosities of the NPS-XG binary pastes taken at constant shear of  $50 \text{ s}^{-1}$

Paste concentration (%)		Average apparent viscosities (Pa s) of the paste prepared at	
NPS	XG	80°C	95°C
2	0	0.243±0.007fg*	0.340±0.006i
	0.010	0.186±0.013g	0.329±0.010i
	0.075	0.144±0.006g	0.402±0.004ghi
	0.150	0.144±0.000g	0.497±0.003fgh
3	0	0.795±0.076d	0.615±0.075f
	0.010	0.575±0.049e	0.516±0.008fg
	0.075	0.368±0.018f	0.435±0.047ghi
	0.150	0.316±0.005fg	0.384±0.015hi
4	0	1.240±0.021c	1.040±0.013c
	0.010	1.093±0.136c	1.045±0.028c
	0.075	0.794±0.065d	0.895±0.045d
	0.150	0.622±0.018e	0.762±0.032e
5	0	1.524±0.193ab	1.476±0.039a
	0.010	1.654±0.140a	1.488±0.025a
	0.075	1.461±0.004b	1.433±0.168a
	0.150	1.143±0.028c	1.258±0.062b

\*Different characters in columns point to statistically essential differences at  $\alpha = 0.05$ .

Also fairly stable in time were apparent viscosities measured involving the in-shear structural recovery test with determination of the degree of structure recovery (Wang *et al.*, 2009; 2010). These values differed from these collected at constant shear rate (Table 3).

Systems with DSR equal to unity are regarded as stable. Careful inspection of Table 3 leads to the finding of two such systems (bolded). These are 4% NPS with 0.010% XG prepared at 80°C and 5% NPS with 0.075% XG prepared at 80°C. The in-shear structure recovery test is a test measuring thixotropy and allows the detection of systems which show stability/instability in time as described in Adamczyk *et al.* (2012). From this point of view, these systems can be compared to modified starches, as they are produced to deliver also stability in time.

In this paper a focus is shown on the possibility of substitution of OS (E1404) with NPS-XG binary mixtures.

The OS pastes were non-Newtonian, shear thinning fluids (Fig. 1a, Table 4). With an increase of their concentration, an increase of the shear stress values (particularly

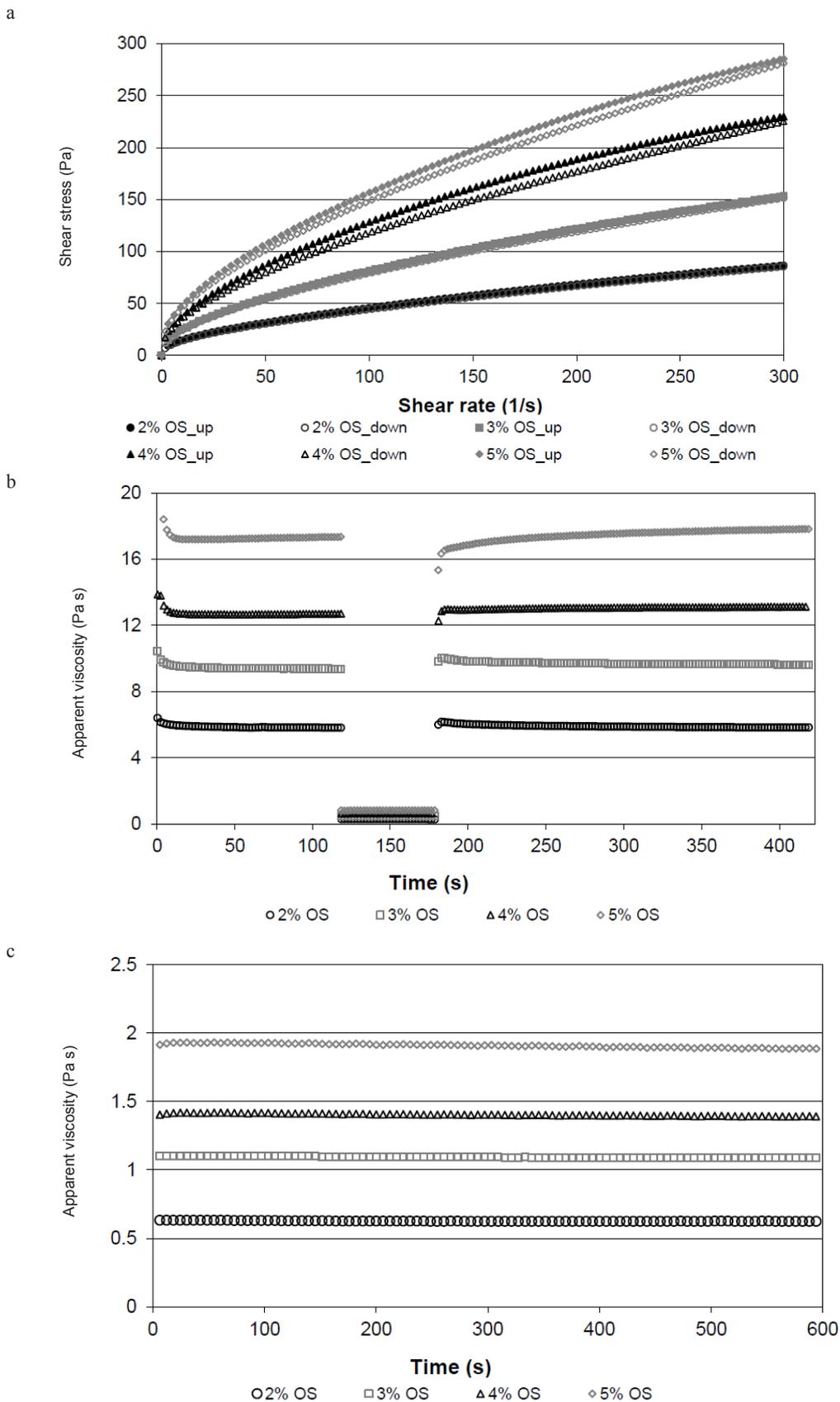
at higher shear rates – Fig. 1a) and apparent viscosities, both at shear rate of  $50 \text{ s}^{-1}$  (Fig. 1c) and in each step of the in-shear structural recovery test (Fig. 1b), was observed. Moreover, in the whole range of the shear rates applied almost all OS pastes demonstrated higher shear stress values compared to those of NPS pastes of the same concentration when pasted at 95°C (Sikora *et al.*, 2015). 3% OS pastes showed similar shear stress to the corresponding NPS pastes. These results are confirmed by the literature (Pietrzyk and Fortuna, 2006; Fortuna *et al.*, 2004), where OS oxidised by sodium (I) chlorate had much lower shear stresses as compared to NPS, which was explained in terms of hydrolysis of the modified starch. Observed differences can result from the different properties of NPS (Sikora *et al.*, 2015) and potato starch used for the production of OS. The increase in the concentration of the OS pastes was accompanied by an increase in consistency coefficient  $K$  (Table 4). Simultaneously, flow behaviour index  $n$  was considerably below unity and it was similar for all modified starch pastes. The consistency coefficients  $K$  of all OS pastes were higher than these for corresponding NPS pastes (Sikora *et al.*, 2015). This confirmed higher apparent viscosity of OS pastes. The samples of OS (excluding 3% OS) had lower flow behaviour index  $n$  than those of NPS (Sikora *et al.*, 2015), which suggests greater non-Newtonian character (the samples were more shear-thinned). The course of the flow curve (Fig. 1a), consistent with the clockwise direction and the values of hysteresis loop areas of thixotropy (Table 4), suggested that the OS pastes had thixotropic properties, the greater the higher the concentration of OS applied. However, such behaviour of the OS samples was not confirmed by the results of the apparent viscosity measurements at  $50 \text{ s}^{-1}$  (Fig. 1c) as well as of the degree of the structure recovery DSR values (Table 4). Small changes of the apparent viscosity during shearing at  $50 \text{ s}^{-1}$  and values of DSR close to 1 indicated a high rheological stability of the OS pastes, regardless of their concentration.

The values of shear stress and consistency coefficient (Fig. 1a, Table 4) allow the assumption that in order to obtain mixed pastes with shear stresses and parameters of the Ostwald-de Waele model similar to those of OS pastes an addition of XG should mainly increase the apparent viscosity and pseudoplasticity of the NPS samples. The values of hysteresis loop areas are less significant as they do not describe the phenomena of thixo-antithixotropy quantitatively (Adamczyk *et al.*, 2012; Barnes, 1997; Steffe, 1996). The more important is an addition of XG to stabilise the pastes, that is the DSR values (Table 3) should be close to 1 as well as changes of the apparent viscosity at  $50 \text{ s}^{-1}$  should be small and their values high (Table 2). Additionally, having in mind the fact that the DSR is the ratio of mean value of apparent viscosity in the first 120 s of the fifth step of shearing to the mean value of apparent viscosity in the third step, samples with similar DSR in reality can significantly

**Table 3.** Average apparent viscosities and the DSR of 2-5% NPS-XG binary pastes taken by the in-shear structural recovery test

Pasting temperature (°C)	XG concentration (%)	Mean apparent viscosity (Pa s)		
		3rd step	5th step	DSR
2% pastes				
80	0	1.87±0.25b*	1.67±0.14de	0.91±0.03c
	0.010	1.93±0.06b	1.53±0.01e	0.80±0.02d
	0.075	2.02±0.11b	1.88±0.12cd	0.93±0.00c
	0.150	2.13±0.02b	2.01±0.02bc	0.94±0.00c
95	0	1.93±0.01b	2.56±0.07a	1.33±0.03a
	0.010	2.16±0.12b	2.21±0.05a	1.04±0.09b
	0.075	2.75±0.08a	2.57±0.08a	0.93±0.00c
	0.150	2.67±0.21a	2.57±0.21a	0.96±0.00bc
3% pastes				
80	0	5.42±0.71bcd	4.48±0.17b	0.84±0.08d
	0.010	4.89±0.47cd	4.44±0.29b	0.91±0.03cd
	0.075	5.81±0.06bcd	5.43±0.06ab	0.93±0.00cd
	0.150	6.03±0.05bcd	5.68±0.06ab	0.94±0.00cd
95	0	4.42±0.11cd	5.83±0.35ab	1.32±0.04a
	0.010	3.99±0.03d	4.74±0.38b	1.19±0.09b
	0.075	7.36±2.18a	7.22±2.16a	0.98±0.00c
	0.150	6.35±0.42bc	6.10±0.54ab	0.96±0.02c
4% pastes				
80	0	8.36±0.18c	9.40±0.255bc	1.12±0.01b
	0.010	10.13±0.06b	10.155±0.63ab	1.00±0.06b
	0.075	11.72±0.43ab	11.305±0.13a	0.92±0.01c
	0.150	11.98±1.12a	11.09±1.10a	0.93±0.01c
95	0	5.31±0.08d	7.235±0.02d	1.37±0.02a
	0.010	5.40±0.18d	7.37±0.11d	1.37±0.02a
	0.075	7.45±1.62c	8.06±1.05cd	1.10±0.09b
	0.150	11.31±0.16ab	10.895±0.06a	0.97±0.02c
5% pastes				
80	0	9.22±1.77c	11.21±1.48bc	1.22±0.08bc
	0.010	8.87±0.89c	10.87±0.89bc	1.23±0.02bc
	0.075	16.43±1.29a	16.48±1.32a	1.00±0.00d
	0.150	17.20±0.66a	16.26±0.64a	0.95±0.01d
95	0	6.70±1.12c	10.00±0.89c	1.51±0.18a
	0.010	8.21±0.82c	11.34±0.67bc	1.38±0.06ab
	0.075	7.59±0.41c	10.33±0.46c	1.36±0.01ab
	0.150	11.68±0.46b	12.68±0.31b	1.09±0.01cd

\*Different characters in columns (for each starch concentration) point to statistically essential differences at  $\alpha = 0.05$ .



**Fig. 1.** Flow curves (a), results of the in-shear structural recovery test with pre-shearing (b) and apparent viscosities at 50 s<sup>-1</sup> (c) of 2-5% OS starch pastes.

**Table 4.** Parameters of the Ostwald – de Waele rheological model and areas of hysteresis loops for 2-5% OS and similar\* results obtained for the mixed NPS:XG pastes

Samples	Parameters of the Ostwald de Waele model**		Area of the hysteresis loop ( $W\ m^{-3} = Pa\ s$ )		
	$K$ ( $Pa\ s^n$ )	$n$ (-)	Thixotropy	Antithixotropy	Total area
Samples of OS					
2%	3.47±0.03c d ***	0.563±0.005ab	125±58bc	4±4b d	129±54b d
3%	6.06±0.14b c	0.566±0.001 b	203±11abc	15±0a d	218±11b cd
4%	10.73±0.67a b	0.540±0.009c b	1091±16a	5±3b d	1096±16a b
5%	12.75±1.53a	0.547±0.008bc	939±446ab	9±2ab d	947±444a bc
Samples similar to 2% OS					
3%NPS+0.010%XG at 95°C	2.15±0.73d	0.643±0.047a	1±1c	443±99c	444±98bcd
Samples similar to 3% OS					
4%NPS+0.010%XG at 80°C	5.52±1.57c	0.562±0.044b	0±0c	884±59b	884±59bc
5%NPS+0.075%XG at 95°C	6.10±0.06c	0.576±0.011b	1±1c	1940±311a	1941±310a
Samples similar to 4% OS					
5%NPS+0.010%XG at 80°C	10.24±0.96b	0.530±0.009b	421±322abc	256±202cd	677±120bcd
Samples similar to 5% OS					
5%NPS+0.150%XG at 80°C	13.05±0.05a	0.369±0.011c	778±950abc	179±244cd	956±706bc

\*Samples selected on the basis of flow curves similarity. \*\* $K$  – consistency coefficient,  $n$  – flow behavior index. In all cases  $R^2 > 0.996$ .

\*\*\*Different characters in columns denote statistically essential differences at  $\alpha = 0.05$ .

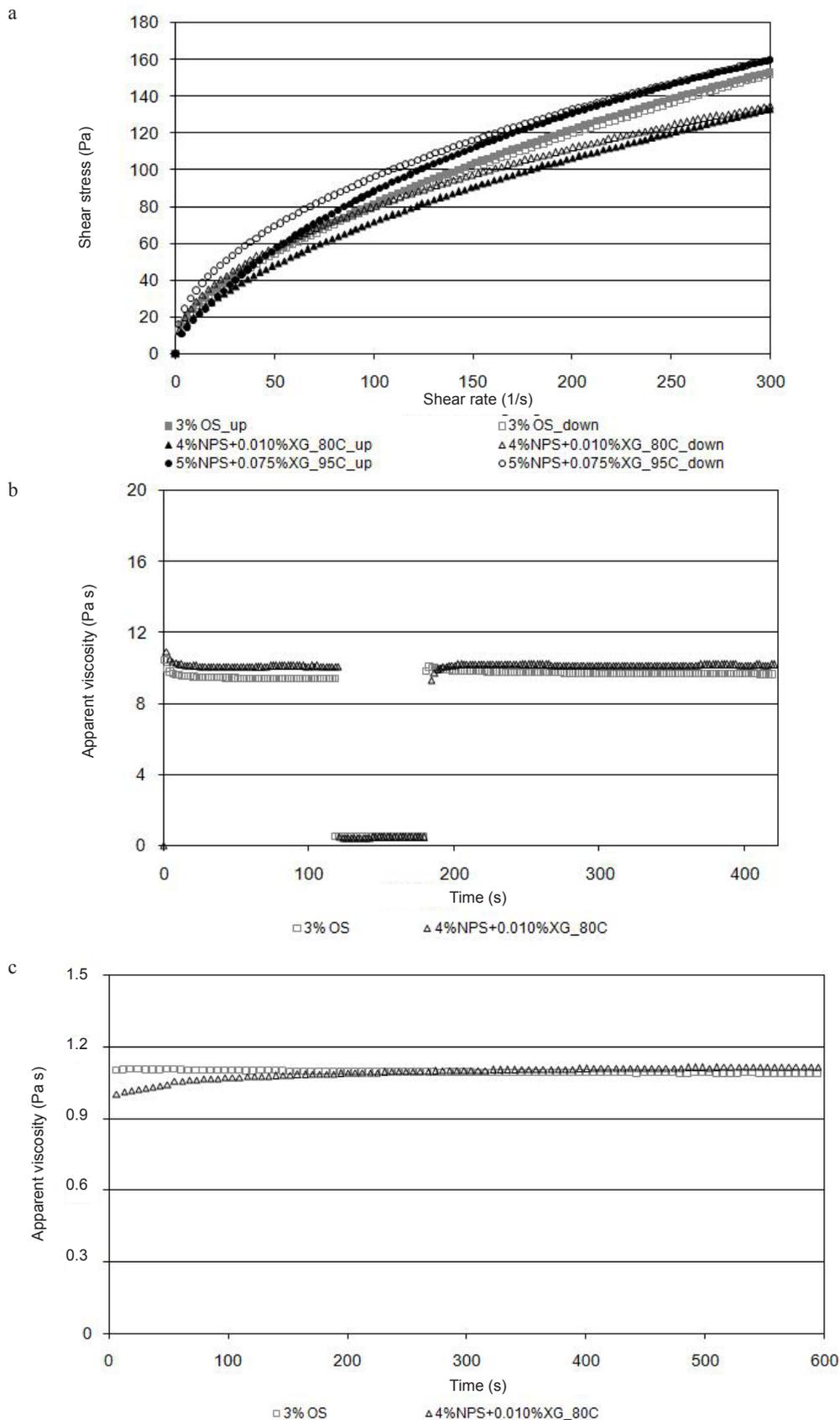
differ from one another with regard to the rheological properties. By reason of this the NPS:XG mixed pastes should have values of apparent viscosity similar to OS pastes in the particular steps of shearing (Tables 2 and 4). This is extremely important in steps 3 and 5 because relatively high values of shear rates evoke higher differences.

Comparisons of the rheological properties of the binary NPS-XG pastes with the properties of the OS pastes brought different results depending on the above mentioned criteria of similarity (Tables 4 and 5). Thus, when the comparisons were made based on the shear stress values and parameters of the Ostwald – de Waele model it was found that 3% NPS paste with 0.010% XG prepared at 95°C best fitted the properties of 2% OS paste (Table 4). Pastes containing 4% NPS paste with 0.010% XG prepared at 80°C and 5% pastes of NPS with 0.075% XG pasted at 95°C exhibited the properties of 3% OS paste (Table 4, Fig. 2a). Apart from that, 5% NPS paste with 0.010% XG prepared at 80°C resembled the properties of 4% OS paste and 5% NPS paste with 0.150% XG prepared at 80°C mimed the properties of 5% OS paste (Table 4).

When apparent viscosities measured at constant shear were regarded, properties of 2% OS paste could be mimed by 3% NPS paste with 0.010% XG prepared at 80°C (Table 5). Also binary 4% NPS paste with 0.010% XG prepared at 80°C was similar to 3% OS pastes (Table 5, Fig. 2 c), as well as binary 5% NPS pastes with 0.010% XG prepared at 95°C, sheared at  $50\ s^{-1}$  (Table 5), had apparent viscosity close to that of 4% AcDP paste. One may see that when apparent viscosity at constant shear rate was adopted as the similarity criterion no combination of NPS with XG could provide a substitute for 5% OS paste.

When apparent viscosity measured by the in-shear structural recovery test was taken under consideration, 3% NPS paste with 0.075% XG prepared at 80°C as well as 3% NPS paste with 0.150% XG prepared at the same temperature best resembled 2% OS paste. Other NPS-XG binary paste substitutes for 3 to 5% OS pastes are listed in Table 5 and/or in Fig. 2b.

Because of intervention of the interaction energy between components of binary pastes and components of thickened system it should be taken under consideration that similarity of rheological and thixotropic properties of



**Fig. 2.** Flow curves (a), results of the in-shear structural recovery test with pre-shearing (b) and apparent viscosities at  $50 \text{ s}^{-1}$  (c) of 3% OS and NPS:XG samples with properties similar to 3% OS pastes.

**Table 5.** Average apparent viscosity in the third and the fifth (in the first 120 s) steps of in-shear structural recovery test as well as the DSR and apparent viscosities at 50 s<sup>-1</sup> of 2-5% OS pastes and similar\* results obtained for the mixed NPS:XG pastes

Samples	Apparent viscosity (Pa s)		DSR	Apparent viscosity at 50 s <sup>-1</sup> (Pa s)
	step 3	step 5		
Samples of OS				
2%	5.88±0.06e*	5.97±0.01d	1.02±0.01ab	0.628±0.011d
3%	9.46±0.10d	9.77±0.07c	1.04±0.01a	1.097±0.028c
4%	12.59±0.11b	12.83±0.11b	1.02±0.00ab	1.410±0.148b
5%	17.41±1.74a	17.17±1.88a	0.99±0.01bc	1.919±0.075a
Similarities in apparent viscosity test				
similar to 2% OS	3%NPS+0.010%XG at 80°C			0.575±0.049d
similar to 3% OS	4%NPS+0.010%XG at 80°C			1.093±0.136c
similar to 4% OS	5%NPS+0.010%XG at 95°C			1.488±0.025b
Similarities in in-shear recovery test (at 80°C)				
Samples similar to 2% OS				
3%NPS+0.075%XG	5.81±0.00e	5.43±0.06d	0.93±0.00d	
3%NPS+0.150%XG	6.03±0.05e	5.68±0.06d	0.94±0.00d	
Samples similar to 3% OS				
4%NPS+0.010%XG	10.13±0.06cd	10.16±0.63c	1.00±0.06ab	
Samples similar to 4% OS				
4%NPS+0.075%XG	11.72±0.43bc	11.305±0.13bc	0.92±0.01d	
4%NPS+0.150%XG	11.98±1.12b	11.09±1.10bc	0.93±0.01d	
Samples similar to 5% OS				
5%NPS+0.075%XG	16.43±1.29a	16.48±1.32a	1.00±0.00ab	
5%NPS+0.150%XG	17.20±0.66a	16.26±0.64a	0.95±0.01cd	

given OS pastes and their binary NPS-XG substitutes taken *in vitro* does not mean that their performance under *in vivo* conditions would also be similar.

Amylose (Am) – amylopectin (Amp) is a system forming a separate phase system in which substantial Am-Amp interactions are lacking (Hermansson *et al.*, 1995; Lii *et al.*, 2002). Nevertheless, at certain Am:Amp proportions in the system a considerable increase in viscosity associated with fair time dependent stability takes place. It could be afforded when the pastes contained either low concentration of Am in Amp or low concentration of Amp in Am.

Such results could suggest that also under such conditions an increased viscosity of NPS-XG binary paste could be afforded.

## CONCLUSIONS

1. Binary mixtures of normal potato starch pastes with xanthan gum, both being anionic polysaccharides, showed an effect of thickening provided the concentration of xanthan gum in normal potato starch did not exceed 0.150%.
2. Temperatures of paste preparation as well as the normal potato starch paste concentration were also factors influencing the thickening effect.

3. All binary systems with 2% normal potato starch pastes prepared both at 80 and 95°C as well as with 5% normal potato starch pastes prepared at 80°C were thixotropic regardless of the concentration of xanthan gum added. The other normal potato starch-xanthan gum pastes were purely antithixotropic.

4. Pastes of oxidised starch had high rheological stability.

5. Rheological properties of some of the binary normal potato starch-xanthan gum blends resemble such properties of pastes of oxidised starch.

6. Rheological properties of binary mixtures can be tailored.

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